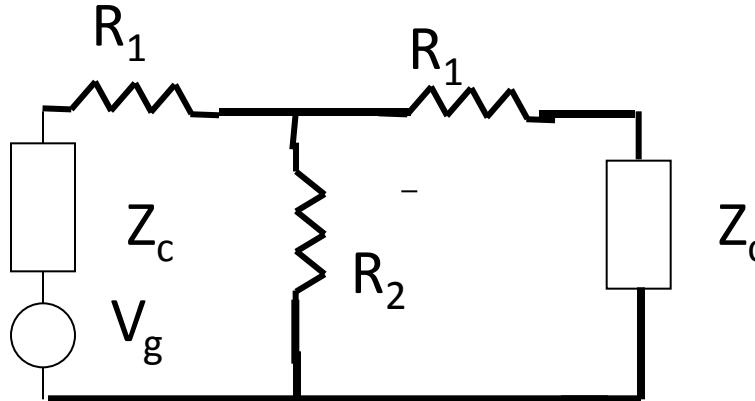


UNIT-2

Microwave Engineering

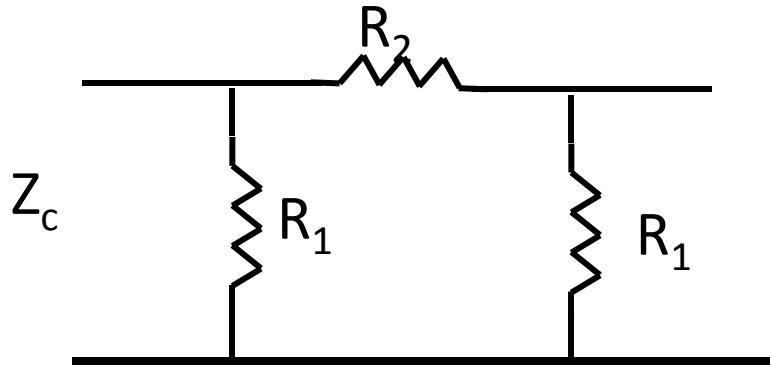
Passive Microwave Devices

Attenuators



T section

$$R_{in} = R_1 + \frac{R_2(R_1 + Z_c)}{R_1 + R_2 + Z_c}$$



π section

$$\text{For } R_{in} = Z_c \Rightarrow R_1(R_1 + 2R_2) = Z_c^2$$

$$V_{TH} = \left(\frac{R_2}{R_1 + R_2 + Z_c} \right) V_g$$

The power delivered to the load is :

$$P_L = \frac{1}{2} \left| \frac{V_{TH}}{2Z_c} \right|^2 Z_c = \left(\frac{R_2}{R_1 + R_2 + Z_c} \right)^2 \frac{|V_g|^2}{8Z_c} = K^2 \frac{|V_g|^2}{8Z_c}$$

$$K^2 = \left(\frac{R_2}{R_1 + R_2 + Z_c} \right)^2 \quad \text{Power attenuation, } R_{in} = Z_c \Rightarrow$$

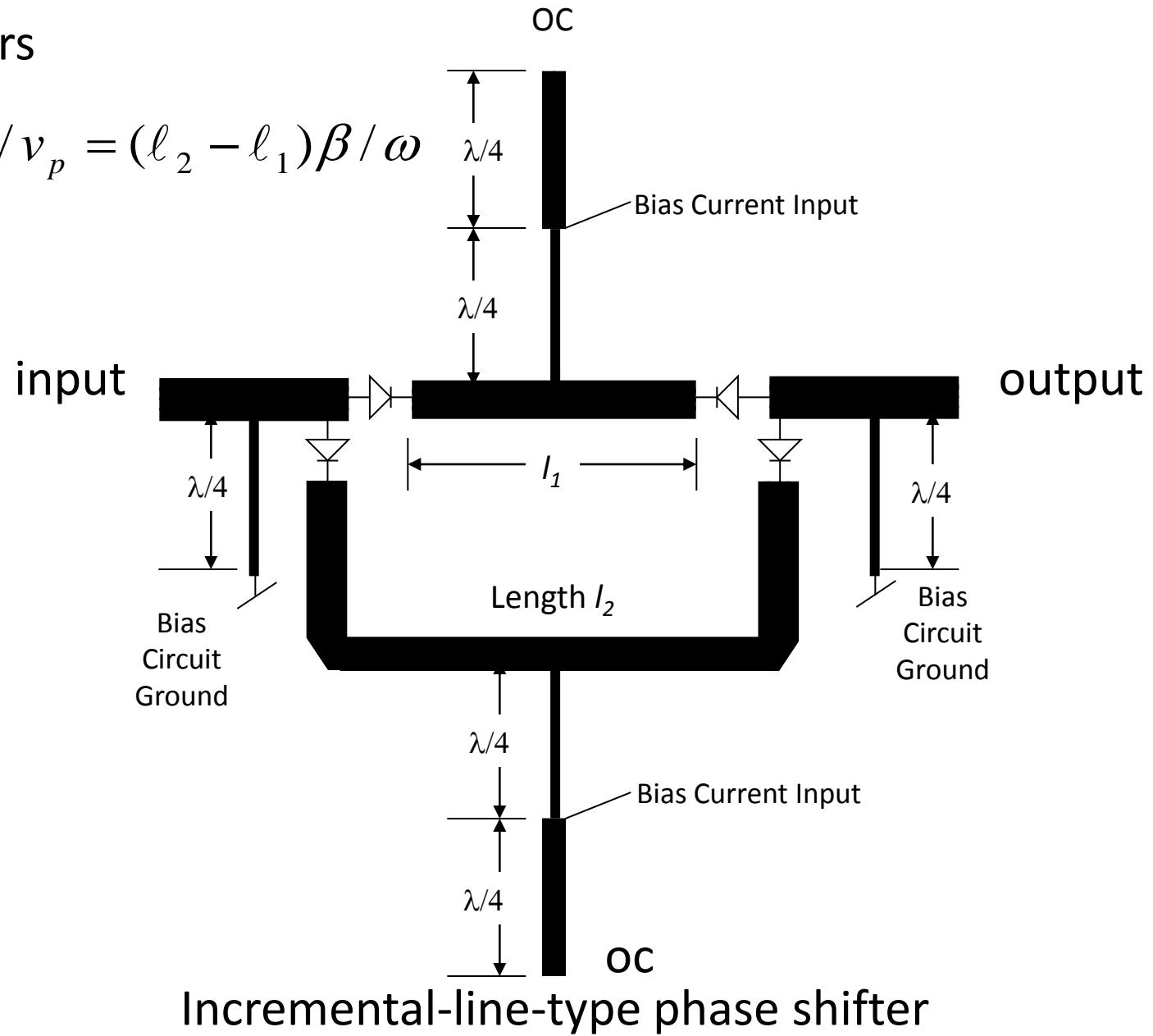
$$R_1 = \frac{1-K}{1+K} Z_c \quad , \quad R_2 = \frac{2K}{1-K^2} Z_c$$

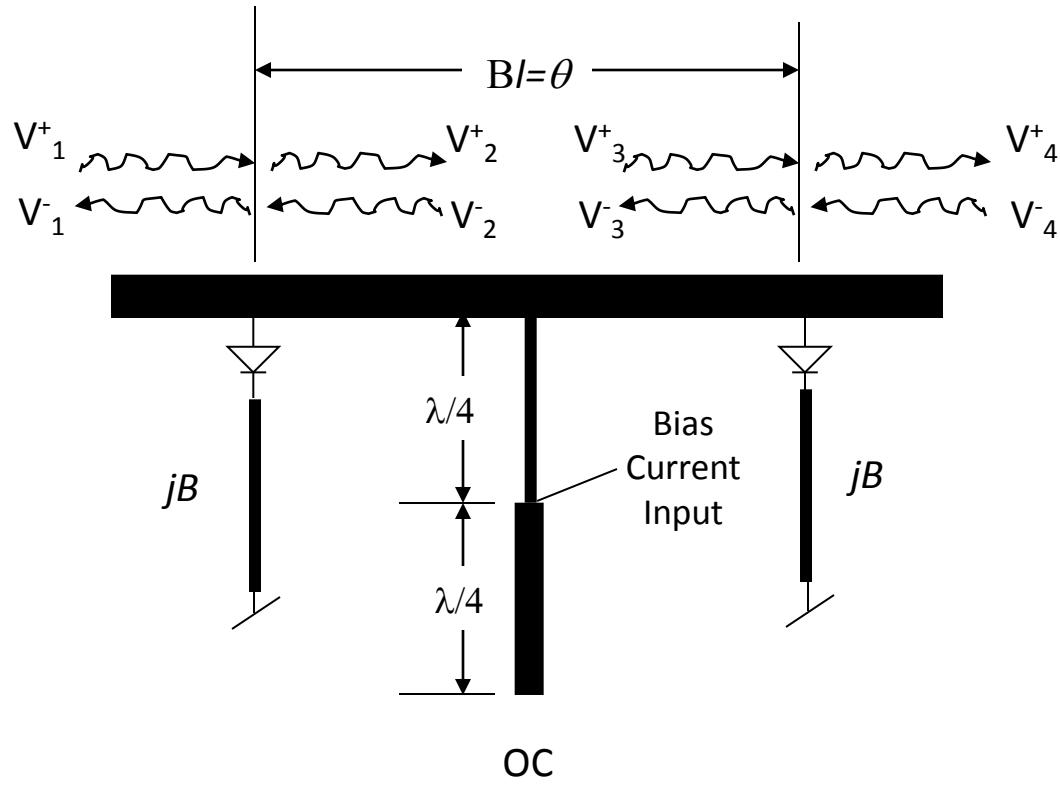
For 3 - dB attenuator $R_1 = 8.58\Omega$, and $R_2 = 141.4\Omega$.

PIN diode can be used in parallel with R_2 in the π - section configuration to switch it in and out of the circuit

Phase shifters

$$\Delta\tau = (\ell_2 - \ell_1) / v_p = (\ell_2 - \ell_1) \beta / \omega$$





A phase shifter using switched reactive elements

Transmission matrix of a normalized shunt susceptance jB :

$$[A_1] = \begin{bmatrix} 1 + j\frac{\bar{B}}{2} & j\frac{\bar{B}}{2} \\ -j\frac{\bar{B}}{2} & 1 - j\frac{\bar{B}}{2} \end{bmatrix}$$

Transmission matrix of a section of transmission line of
Electrical length θ :

$$[A_2] = \begin{bmatrix} e^{j\theta} & 0 \\ 0 & e^{-j\theta} \end{bmatrix}$$

Relationship among wave amplitudes:

$$\begin{bmatrix} V_1^+ \\ V_1^- \end{bmatrix} = \begin{bmatrix} A_1 & \\ & A_2 \end{bmatrix} \begin{bmatrix} V_2^+ \\ V_2^- \end{bmatrix} = \begin{bmatrix} A_1 & \\ & A_2 & \\ & & A_3 \end{bmatrix} \begin{bmatrix} V_3^+ \\ V_3^- \end{bmatrix} = \begin{bmatrix} A_1 & \\ & A_2 & \\ & & A_3 & \\ & & & A_4 \end{bmatrix} \begin{bmatrix} V_4^+ \\ V_4^- \end{bmatrix}$$

$$= \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} \begin{bmatrix} V_4^+ \\ V_4^- \end{bmatrix}$$

Choose $V_4 = 0$, then $V_4^+ = V_1^+ / A_{11}$ Thus $T_{14} = 1 / A_{11}$

$$T_{14} = \left[\left(1 + j \frac{\bar{B}}{2} \right)^2 e^{j\theta} + \frac{\bar{B}^2}{4} e^{-j\theta} \right]^{-1}$$

If $\tan \theta = 2/\bar{B}$ then : $T_{14} = -e^{j\theta} = e^{-j(\pi-\theta)}$, $|T_{14}| = 1$

$$\Delta\Phi = (\pi - \theta) - \theta = \pi - 2\theta$$

$$\text{For } \bar{B} = 2, \theta = \pi/4, \quad \Delta\Phi = \pi/2$$

$$\text{For } \bar{B} = 1, \theta = 1.107, \quad \Delta\Phi = 53.14^\circ$$

Choose the two stubs such that $j\bar{B}_2 = -j\bar{B}_1$

$$T_{14} = \left[\left(1 + j \frac{\bar{B}}{2} \right)^2 e^{j\pi/2} + \frac{\bar{B}^2}{4} e^{-j\pi/2} \right]^{-1} = -j \left[1 + j\bar{B} - \frac{\bar{B}^2}{2} \right]^{-1}$$

$$\approx -j(1 + j\bar{B})^{-1}$$

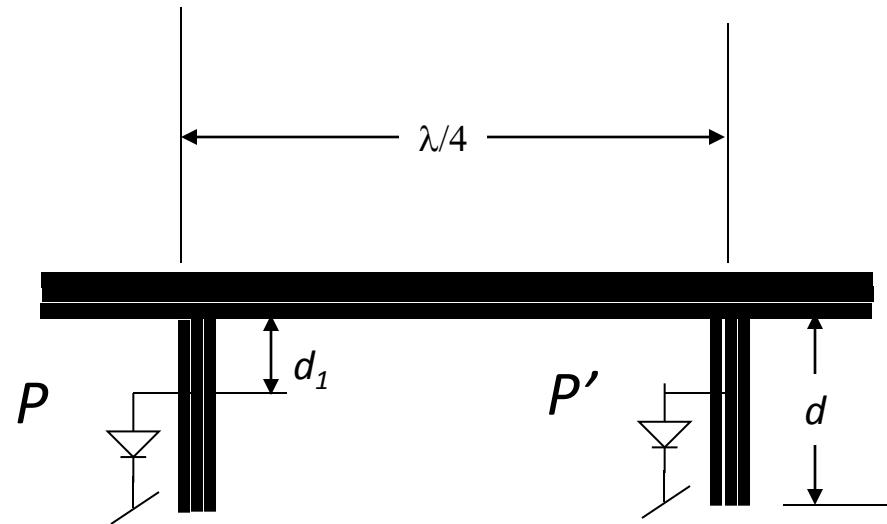
When $\bar{B} \ll 1$, $|T_{14}|^2 = (1 + \bar{B}^2)^{-1} \approx 1$

Phase of $T_{14} = -\pi/2 - \tan^{-1} \bar{B} \approx -\pi/2 - \bar{B}$

The change in phase when $\bar{B} = \bar{B}_1$ and $\bar{B} = -\bar{B}_1$ is $2\bar{B}_1$

A value of \bar{B}_1 as large as 0.2 $\Rightarrow \Delta\Phi = .4 = 22.92^\circ \Rightarrow$ large mismatch.

This phase shifter is limited to small phase shifts between states in order to keep the input VSWR small



A phase shifter using open circuited stubs spaced $\lambda/4$ Apart. P and P' are switched into the circuit when the Diodes are off and on, respectively.

$b_1 = 0$ port 1 is matched , $b_2 = 0$ port 2 is decoupled

$\Gamma_e = \Gamma_o = 0 \Rightarrow \bar{A} + \bar{B} = \bar{C} + \bar{D}, \quad \bar{A} = \bar{D}$ for both even and odd modes,

then $\bar{B} = \bar{C}$ or : $\bar{Z}_{02} = \frac{\bar{Z}_{01}}{\sqrt{1 - \bar{Z}_{01}^2}}$

$$T = \frac{1}{\bar{A} + \bar{B}}, \quad T_e = -\sqrt{1 - \bar{Z}_{01}^2} - j\bar{Z}_{01} \text{ and } T_0 = \sqrt{1 - \bar{Z}_{01}^2} - j\bar{Z}_{01}$$

$$b_4 = -j\bar{Z}_{01}a_1 \quad \text{and} \quad b_3 = -\sqrt{1 - \bar{Z}_{01}^2}a_1$$

$$\text{Coupling} = 10 \log \left(\frac{1}{1 - \bar{Z}_{01}^2} \right), \text{ since } P_3 = b_3^2 \text{ and } P_1 = a_1^2$$